Technical Report Documentation Page

1. Report No.	2. Government Acces	sion No.	3. Recipient's Catalog N	lo.
FAA-AM-78-23				
4. Title and Subtitle			5. Report Date	
GPSS COMPUTER SIMULATION OF EMERGENCY EVACUATIONS	AIRCRAFT PASS		6. Performing Organizati	
7. Author's)			8. Performing Organization	on Report No.
J. D. Garner, R. F. Chandle	er, and E. A. (Cook		
9. Performing Organization Name and Addres			10. Work Unit No. (TRAI	S)
FAA Civil Aeromedical Insti	ltute		11. Contract or Grant No	
Oklahoma City, Oklahoma 73	3125		13. Type of Report and F	'eriod Covered
12. Sponsoring Agency Name and Address Office of Aviation Medicine Federal Aviation Administra	ation			
800 Independence Avenue, S.	. W .		14. Sponsoring Agency C	ode
Washington, D.C. 20591 15. Supplementary Notes				
Research leading to prepara Task AM-B-77-PRS-53.	ation of this 1	report was condu	icted under	
16. Abstract				
The costs of civil air transubjects have risen as seat Repeated tests further inconarticipants.	ing capacities	s of these airc	raft have increa	sed.
A method to simulate such estatistics from measured control this model uses the General language to represent various exit configurations, passer slide capacity, and redirect	omponents of the Purpose Simulous features of ager mix, door-	ne escape path, Lation System (C f the escape pro -opening delays	has been develoges) computer pocess; e.g., sea, time on escape	oped. Programing Sting and Salides,
Results of simulated evacua a military aircraft are rep of certification demonstrat of exit size substitutions escape potential for exit of	oorted. These tions from the were evaluated	results have be DC-10, L-1011, as a means of	een compared wit and B-747. Com	th results oparisons
17. Key Words		18. Distribution Statem		
Evacuation simulation Escape Computer model		through the Na	vailable to the ational Technica ngfield, Virgini	1 Information
				1
19. Security Classif. (of this report)	20. Security Clas		21. No. of Pages	22. Price
Unclassified	Unclassi	f ie d	16	

```
MEAN = 1.57 SD = 0.76 FORWARD EXIT TIME FUNCTION

1 FUNCTION RN3,C32 FORWARD EXIT FUNCTION (TYPE I)

0,0/.00132,20/.01662,40/.06162,60/.13949,80/.24221,100/.35722,120
.47262,140
.57971,160/.67340,180/.75173,200/.81485,200/.86423,240/.90190,260/
.93005,280/.95070,300/.96562,320/.97625,340/.98373,360/.98894,380/
.99254,400/.99500,420/.99667,440/.99779,460/.99854,480/.99904,500/
.99937,520/.99959,540/.99974,560/.99983.580/.99989,600/1.0000,700

* MEAN = 1.73 SD = .45 FORWARD SLIDE TIME
```

Figure 1. Example of the forward Type I exit function.

that elongates the top of the curve. Each evacuation pathway segment in the model references similar functions for random selection of passenger movement; i.e., time in each segment, until the passenger is on the ground.

The model limits the number of passengers allowed to occupy specific escape slides at one time to three on a single-lane slide, six on a double-lane slide, or to other numbers designated by the user. The length of an escape slide corresponds to the time-on-the-slide function in the model and, consequently, a delay could result in the rate at which passengers may enter the top of the slide.

The model has the capability to use differing mathematical routines, if needed, although none were used in this report. Such routines would be entered into the input listings along with the functions now used.

Transactions are accumulated in counting blocks that register passenger times, numbers of occupants using a facility (door, slide, etc.), and cumulative data during evacuations for each segment of the escape route. These data are then printed out in tabular or graphic form. The redirection of passengers in the cabin from longer waiting lines to an adjacent exit with shorter queues depends on the number programed for the shorter line to contain before transfers take place. The model assumes that passengers reach the shorter exit line before a gap in the escape line occurs. This exit reassignment is similar to volunteer passenger transfers that take place in evacuation demonstrations.

The time at which the last person reaches the ground at each exit is defined as the evacuation time, and the time at the exit with the longest evacuation time is defined as the total escape time. A number of runs on a particular configuration can be made to permit random selections to represent human performance variables on each run and to enable statistical statements of evacuation predictions. Runs of 10, 20, 40, 50, and 100 repeated model evacuations were examined to assess the number of runs needed to confidently display the built-in randomness. The optimum number of runs to allow adequate distribution appears to be between 20 and 40. For each configuration, 20 evacuations were made during the majority of the developmental simulations; this number appeared to provide satisfactory results.

Model Input Data Sources. A central source to obtain all evacuation data relating to transport aircraft does not exist. The aircraft manufacturers, airlines, FAA headquarters and field offices, the National Transportation Safety Board, and the Evacuation Research Unit at the Civil Aeromedical Institute (CAMI) each have limited information. The largest publication thus far is of data assembled by the Aerospace Industries Association (AIA) in their study of evacuations in 1967-68 (4). Assembly and publication of similar data since 1968 has not been accomplished but would be desirable to support the selection of quantitative data for computer inputs. This is especially true since most wide-bodied aircraft were evacuation certified during the early 1970's and are not included in the earlier AIA report.

Passenger flow rates through Type I (24 x 48 in) and Type A (42 x 72 in) exits, described in the Federal Aviation Regulations (25.807), and used in the GPSS model, were derived from the results of an evaluation performed by CAMI in Oklahoma City (5). Overall flow rates through Type I exits averaged 46.8 passengers/min or 1.28 s/passenger. The overall rate for the Type A exit averaged 126.2 passengers/min or 0.48 s/passenger. A ratio of 2.6 has been used for Type A exit escape rates and appears in the GPSS as 10/26. The computer derives the Type A flow rate by dividing the mean Type I flow rate, entered as parameter function 1 (1.57 s/passenger), by 2.6, which maintains the ratio. The resulting Type A flow rate is 0.60 s/passenger and remains in use in the GPSS program until a more representative rate is established for validation of the model.

Calculation of passenger flow rates during the evacuations can be performed either by using the total time from test start to the last out or by considering the time from the first passenger out until the last has evacuated.

Thus, the overall flow rate for an exit is defined by the following ratio:

Time (s) from start signal
to last passenger on ground = Average overall flow rate
No. passengers evacuated (s/passenger)

Continuous flow rate is defined as:

Time (s) from first passenger on ground to last passenger on ground = Average continuous flow rate No. passengers - 1 (s/passenger)

GPSS General Format. Appendix A is a typical GPSS evacuation program showing the analysis of 527 passengers evacuating a B-747 aircraft through five Type A exits. The first entries in Appendix A, four statements of model operational instructions, are followed by seven Function entities. The Functions permit computations of discrete functional relationships between an independent variable and dependent values of the function. For the B-747 evacuation, these functions are probabilistic distributions from which random

Table 2 lists results of a series of six simulated evacuations, each the average of 20 runs, on the L-1011 aircraft with 356 or 411 passengers. The objective of the runs was to comparatively evaluate a Type I exit vs. a Type A exit in the aft exit position in combination with three other Type A exits on the L-1011. Three of these simulations were comparable to aircraft evacuation demonstrations, the results of which are noted for comparison in Table 2.

TABLE 2. Evacuation Times and Conditions of GPSS Simulation of an L-1011 Evacuation (20 Computer Runs; Exit-Opening Time = 13 s)

No.	Exit	s Used	Intrad Redire	cabin ection	Average Total Evacuation Time	Average Total Evacuation Time
Pax.	Α	I	Yes	No	(s)	(Range (s)
356 356	3	1 1	- Y	N -	93.5 ¹ 84.9 ²	77.4 - 120.0 77.8 - 90.8 77.6 - 89.3
356 356	4 4	_	- У	N -	83.6 79.6	76.7 - 83.9
411	4	-	-	N	83.6	77.6 - 89.3
411	4	-	Y	-	79 . 6 ³	76.7 - 83.9

ITotal evacuation time for an actual demonstration was 101.1 s.

Table 3 consists of groups of 20 simulation runs and shows the total average escape times on a DC-10 with 391 passengers with two variables in the simulated conditions. Exit No. 2 (Type A) simulated a delayed exit-opening time of 50 s, with and without redirection of passengers in the cabin. The other variable shown is a blocked aft exit (Type A), with and without redirection.

TABLE 3. Evacuation Times and Conditions of GPSS Simulation of a DC-10 (20 Computer Runs; 391 Passengers)

Exits	Used		cabin ribution	Average Total Evacuation Time	Average Total Evacuation Time	Exi	t - 0pei (s)	_	Time
<u>A</u>	I	Yes	No	(s)	Range (s)	1	2	3	4
3	1	-	N	112.0 92.5	100.0 - 122.0 88.9 - 96.6	13 13	50 50	13	13 13
3	1	Y	-	92.3	88.9 - 96.6 85.8 - 93.2	13	50	13 13	13
3 2	1	-	N N	85.0 144.0	76.0 - 99.0 130.0 - 162.0	13 13	13 13	13 13	13 *
2	1	Y	**** TA	114.0	110.0 - 118.0	13	13	13	*
3 3	1 1	Y Y	-	82.0 90.2	77.0 - 88.0 85.8 - 93.2	13 13	13 13	13 13	13 13

^{*}The aft Type A (Exit 4) was blocked.

²Total evacuation time for an actual demonstration was 82 s.

³Total evacuation time for an actual demonstration was 89.7 s.

Table 4 lists three sets of 20 evacuation simulations that compare evacuation times for: (1) 355 passengers through three Type A and either a Type I (24 x 48 in with a single slide) or a Type B (32 x 72 in with a double slide) exit in the forward position, and (2) 375 passengers through three Type A exits and a Type B exit in the forward position.

TABLE 4. Evacuation Times and Conditions of GPSS Simulation of a DC-10 to Compare Type I and Type B Exit Times (20 Computer Runs)

Exit	ts Us	sed	No.	Intrac Redire		Average Total Evacuation Time	Average Total Evacuation Time
<u>1</u> 1	A	в2	Pax	Yes	No	(s)	Range (s)
1. - -	3	- 1 1	355 355 375	- - Y	N	106.0 58.0 73.4	94.0 - 119.0 55.0 - 61.0 67.9 - 79.4

¹Single-lane slide used.

Special Applications of the GPSS Evacuation Model. The GPSS model was used to simulate a unique evacuation of 114 passengers from a military command post aircraft. In lieu of flight attendants, military personnel working aboard the aircraft at other duties were assigned to prepare the exits for evacuation. The time required for them to reach the exits from their respective work stations was added to door/slide preparation time. Groups of 25 passengers were evacuated from each exit, one exit at a time, to obtain basic input data for statistical controls. The test results (Table 5) were applied to the flow rate determinations for computer functions. Results of simulated evacuations through five and nine Type A exits are shown in Table 6. The total evacuation times and number of passengers out each exit were averaged from 50 computer runs for each exit configuration.

²Double-lane slide used.

TABLE 5. Evacuation Time-Path Data Obtained From Evacuations of 25 Passengers From a Military Command Post Aircraft

Test No.	Exit	Time to Exit (s)	No. Pax Out Exit	Time 4th Pax Out Exit (s)	Time 8th Pax Out Exit (s)	Time Last Pax Out Exit (s)
						
1	L-2	7.1	9	22.2	25.5	27.0
2	L-1	6.8	9	22.2	24.6	26.0
3	R-1	9.2	9	24.0	27.0	28.5
4	R-2	5.3	16	21.0	24.3	31.5
5	L-3	9.2	16	25.2	30.6	42.0
6	R-3	5.4	16		20.4	30.0
7	R-4	6.8	16	23.4	29.4	40.5
8	L-5	9.6	16	24.0	29.4	40.0
9	R-5	5.6	9	25.2	31.2	33.0

TABLE 6. GPSS Computer Model Evacuation Simulation Results: Escape by 114 Passengers From a Command Post Aircraft via 5 and 9 Exits

Exit	Total Evacuation Time (s)	Average No. Evacuees Through Exit
	<u>5 Exit</u>	
R-1	35.34	23.1
R-2	36.72	25.5
R-3	39.45	23.2
R-4	34.70	22.9
R-5	32.47	19.3
	9 Exit	S
R-1	28.90	12.4
R-2	31.49	11.4
R-3	36.33	11.8
R-4	28.37	12.7
R-5	28.37	13.2
L-1	28.10	13.2
L-2	28.82	13.4
L-3	35.88	12.6
L-5	28.80	13.3
- J	20.00	

A second use of the GPSS evacuation model was as a new aircraft design tool. Two exit configurations and three passenger loads for each configuration were presented for exit optimization in a new civil air transport aircraft. The existing five-exit model program was adjusted to a three-exit program by bypassing operational statements for two nonessential exits. Three Type A exits, and one Type I and two Type A exits in combination, were evaluated, each with 208, 248, or 309 passengers. Table 7 displays the evacuation times for the exit combinations and load factors given. It can be seen that 30 percent less time was required for evacuation with the three Type A exits.

TABLE 7. Averages of Evacuation Times for Exit Combinations and Passenger Load Factors Proposed for a New Design Transport Aircraft (20 Computer Runs)

Exits	used .		
<u>I</u>	A	Average Evacuation Time	s (s)
		208 No. Pax 248	309
1 0	2 3		.20.40 83.32

The chart listing the number of passengers using each exit demonstrates the effect of passenger transfers to exits with faster escape rates. The transfers are particularly evident with the smaller Type I exit in the forward position combined with two Type A exits when compared with the configuration of three Type A exits as shown in Table 8.

TABLE 8. Effect of Passenger Transfers Showing Average Number Out Each Exit (20 Computer Runs)

No. Pax		E	xits	
208 248 309		Forward 68.65 82.48 102.48	3 Type A Overwing 71.22 83.10 104.04	Aft 68.13 83.42 102,48
	1 Type	e I and 2 Ty	уре А	
	Forward	Overwing	Aft	
208	42.75	95.75	69.50	
248	51.00	114.28	82.72	
309	63.68	140.95	104.37	

IV. Discussion.

The program of civil air transport evacuation simulation was undertaken to provide a better understanding of the factors that influence evacuation. Existing certification procedures for demonstrating the safe evacuation potential of an aircraft have proven costly and may result in injury to the participants. The present simulation model program is designed with the exit and slide segments of an evacuation as the major determining factors for total evacuation times. In addition, redistribution or reassignment of passengers to equalize waiting lines to escape contributes significantly to the total evacuation time and this is included in the program. The effects of adverse conditions, such as smoke, fallen ceiling panels, and debris in the aisles, on evacuation times have not been simulated because of the lack of available data for any specific condition.

The knowledge gained from the evacuation demonstrations and accident histories has provided a valuable source of information on which judgments for simulation can be based. Criteria must be determined for the simulation that will provide assurance of adequate escape potential from civil transport aircraft and detect factors inimical to escape and survival. The GPSSlanguage computer model has the potential to simulate much more sophisticated entities than are shown in this report. An example is the inclusion of the effects of crew effort on evacuation times. Graded on a scale from 1 to 10, a Factor could be entered that would directly influence passenger flow rates through an exit. Computer runs could be made with both easy and low effort (grade 1) to the most enthusiastic effort (grade 10) to evaluate the effects of crew effort. Of course, data would be required to establish the delay function of the Factor. Another example would relate to exit design evaluations to establish optimum distances between exits while considering exit capacities to provide optimization of a total aircraft exit configuration. Until encumbrances on passenger movement to exits override the limiting flow rates, modeling exit flow and escape slide patterns will provide adequate evacuation performance evaluations. Although some rudimentary information is available on interior cabin movement by individual passengers, group tests will be required to substantiate data for more precise simulations.

V. Conclusions.

- 1. The capability and potential of the GPSS evacuation model have reached the stage in development that allows it to closely simulate actual evacuations from current transport aircraft. With refined inputs, based on additional test results, the model may provide a valid means to certify evacuation systems or evaluate escape system designs while the aircraft are in the early planning stages.
- 2. A group knowledgeable in evacuation simulation should develop a program to provide the data and formulate simulation criteria for potential use as a certification and/or design tool.

- 3. All evacuation tests, research, and actual performance data should be assembled at one source and analyzed to obtain pertinent material for model input functions.
- 4. A final model should be refined and subjected to a rigorous validation process.
- 5. A practical, validated, evacuation simulation model should then be considered for acceptance as a certification and/or design tool.

REFERENCES

- Folk, E. D., J. D. Garner, E. A. Cook, and J. L. Broadhurst: GPSS/360 Computer Models to Simulate Aircraft Passenger Emergency Evacuation. FAA Office of Aviation Medicine Report No. FAA-AM-72-30, 1972.
- 2. General Purpose Simulation System/360 User's Manual, IBM Application Program H20-0326-2. IBM World Trade Corporation, NY, 1968.
- 3. Gillespie, J.: Emergency Evacuation Computer Simulation Program Description and User's Guide. FAA Engineering and Manufacturing Branch Report No. FAA-216-76A, 1976.
- 4. Evacuation, Crashworthiness Development Program Technical Group Report, Aerospace Industries Association of America, Inc., Washington, D.C., 1968.
- 5. Garner, J. D., and J. G. Blethrow: Evacuation Tests From an SST Mock-Up. FAA Office of Aviation Medicine Report No. AM-70-19, 1970.
- 6. Blethrow, J. G., J. D. Garner, D. L. Lowrey, D. E. Busby, and R. F. Chandler: Emergency Escape of Handicapped Air Travelers. FAA Office of Aviation Medicine Report No. FAA-AM-77-11, 1977.

APPENDIX A

TYPICAL GPSS EVACUATION PROGRAM

	GENERATE	*** 527,110		
	TRANSFER	. Zuc. FWDA	A EXII EXPECTS	
	TRANSFER	.250,, *IDA	X W	
	TR AN SF ER	. 333, AFTA		
	TR AN SP FIR	. 50C, , 4FII		
	TAIN SFER	, AJÜL	FIFTH TYPE A EXIT EXPLCTS 1/5	
FWDR	ASSIGN	4,1		C8160740
	ASSIGN	21 6	NER ASSIGNED	C6160750
	ASSIGN	6,12	OPPLSITE SIDE EES NBK ASSIGNED	CB163750
	ASSIGN	9,21		C6100770
	ASSIGN	10,22		CB160780
	ASSIGN	7.1		
	18 ANDFER	, EXIT		Cb160790
A1 آ1-	ASSI UN	1.1		Le160800
	ASSIGN	5,5		CB160810
	4.01884	C 4 3		CE1c0820
	4551 GN	7,24		C8160830
	ASSI SV	10,25		CB1c0340
	ASSION	1,2		
	TRANSFER	, EXIT		CB160850
AFTA	ASSIGN	4.7		CB160860
	ASSIGN	543		C8160870
	ASSIGN	6,3		CB160880
	ASSI 6:4	7,5	OVERMING-KAMP PATH IS NUMBERED 6 IN PT	C81c0890
	ASSIGN	9,27		C6160900
	ASSI GN	10,23		C8163910
	ASSIGN	1,3		
	TRANSFER	PEXIT		CB160920
AFFI	ASSIGN	4 pt t		CE16093U
	ASSIGN	5,11		CE160940
	ASSIGN	5,11		C8160950
	ASSIGN	9,30		CE160960
	ASSIGN	10,31		01609181
	ASSIGN	1.1		
	TK 4/4/5/FFF	• Ex11		CB160980
ADOL	ASSI GN	6144		08609180
	ASSIGN	5,14		Cp1¢1000
	ASSIGN	6,14		CB161010
	ASSIGN	9,33		C8161020
	ASSI GN	10,34		CB161030.
	ASSI GN	2,1		
		, Exit		CB161040
EXIT		M2,114		
P ∈ GIN	ENTER	4	DOORS	
	ADVANCE	FN2	DEOR-MECHANISM DELAY, USING P4 ALSO	C8161120
	LEAVE	P 4		CB161130
	port	X		C8181140
	LINK	PI, FIFU, AAA		

		7 data H		
	16.5T GE	0#9*Ko* SE Z	C5161170	
	17. ST 17.	P 9, 21, MCUM.	Cb161180	
	11 (A) 12 (A) 14	プレッス・ナット しょうしゅん アンドラ アンドラ アンドラ アンドラ アンドラ アンドラ アンドラ アンドラ	C61c1190	
	10.01 10.01 10.01 10.01 10.01 10.01	AMODRAL ZANA	C6161200	
	100 E	- TH-07-77-10-10-10-10-10-10-10-10-10-10-10-10-10-	(6161210	
NOON	TE ST	4×V DO IOE2 FOO CNET	068141930	
		*AS642	C5101530	
<u>နှံ့</u>	- '	£*V*SIJE+*KO*SEZ	Cb461240	
0. 40%	TANSFER OF THE	サンクトでは、これでは、これでは、これでは、これでは、これでは、これでは、これでは、これ	CB161250	
5	•	ようしゅうしゅう ロットラン ロットロットロットロットロットロットロットロットロットロットロットロットロットロ	CB161260	
F)K.	Test E	4.4.5.1.0.1.2.1.2.1.2.1.2.1.2.1.2.1.2.1.2.1.2	CBIE1270	
	TRIAN SECK	1 NO SY 1	0077770	
F JK4	TEST E	C#V#VIOE4*NO*SE2	CC22230 CB161300	
7	TANSFOR THE TANSFORM	▶ ASCAL	CB1c1310	
100		6.4 V # 0.1 OF 1. * K O * 0.5 V Z	CE161320	
SEV	,-	マン・コン・コン・コン・コン・コン・コン・コン・コン・コン・コン・コン・コン・コン	C8161330	
!			C61C1340	
54.43	_	17.00 TO 10.00 TO 10.	C8:61350	
	TX A'N SF CK	+ A > G N 3	(8141436	
Së V4		2 *V*S IUC++AO+SE. Z	O SETATO	
		* # 5 6 4 4		
.≯ ALON		Q*V*SICE1,*KO,TEN2		
:	TRANSFER T. CT	* ASGN1	CB161390	
71:11	10 0 1 C	STANDER TO THE STAND A THE STAND A STA		
TFI	TENT :			
	TRANSFER	**************************************	C6161400	
THION	_	**************************************	C816141U	
1	THAN SFER	• ASGN1		
STEL	TEST E	L*V*SIUES*KU*SEZ		
7.74		22		
7.50	A 6.64.58	ATTO SEND PAX TO MEXT EXIT FORWARD	CB161420	
	A 2 5 1 5 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	5 6 1 4	CE161430	
	CEPAKT		LB101440	
	ASSIGN	F - 6	CB161450	
	QUEUS	54	C5161460	
	CUEUE	P10	C819140	
	Dr.PAK I	P#4	00710100	
			CB161500	
A S CN Z		44+3 SEND PAK TO NEXT EXIT AFT	CB161510	
	NO 1004	5443	CB161520	
	PO I COLL	± φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ	C6161530	
	# 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		CB161540	
	DUEUE	ור היים מיים	Criti550	
	CUEUE	010	CB161560	
	DEPART	610	CB161570	
	TRANSFIR	74.	C8161580	
A SGN 3	_	1 0 1	CB1 01 590	
		42.4	CB161600	
			FR1 x1x1A	

	DEPART	,		010100
	ASSIGN	36		CB161640
	LUEUE	.5d		CB161650
	CUECE	P10		CB161660
	DEPART	P 10		CE161670
	TRANSFER	7 75 1		CB161680
4 NOS A	_	4+16		CB161090
		24,6		CB161700
	ASSIGN	0+16		CB161710
	UEPART	64		CB161720
	ASSION	7++6		CB161730
	OUT UE	5 d		C8161740
	u UE UE	P10		Cp161750
	UEPAKT	P 1:3		CBIOI TOU
	TRANSFER	, Sf 2		CB161770
5 - 2 2	GUE UE	7.5	BEGIN EXIT DELAY-INTERVALS	CB161780
	SE 1 25	J J		CE161750
	CEPAKI	54		CEICISCO
	FAKK	ဆ		CB161810
	ACT VANCE	۷#5		CB1c1820
	VELEASE	or RV		
	TEST F	P4,7,3UE4	PATH 7 INCLUDES OVERWING SEGMENT, 6 IN P7	
	ASSIGN	7,0		CETEISCO
	SOROS	. Ld		C8161870
	ENTER	7 d	ENTER STURAGE FOR OVERWING RAMP	CB161880
	ADVANCE	V#7		CB161890
	LFAVE	1 д		C31¢1900
	DEPART	Ь7		CE161910
4900	JUEU E	74		(61c1920
	ENTER	ر د	ENTER STORAGE FUR SLIDE TIME	CB161930
	AU VANCE	†* >		CB101940
	LEAVE	۳ *ر		C8161950
	DEPART	47		CE161960
	CEPART	7,		CB161970
	SAVEVALUE	7. V. R.	RECURD THE LATEST TUTAL TIME FUR EACH PATH	Ca161990
15'R	TERM INATE			CB162000